

SLOVENSKI STANDARD SIST ISO 16889:2001

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Hydraulic fluid power filters -- Multi-pass method for evaluating filtration performance of a filter element

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Filtres pour transmissions hydrauliques - Évaluation des performances par la méthode de filtration en circuit fermé

SIST ISO 16889:2001

Ta slovenski standard je istoveten z: 150-16889:1999

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INTERNATIONAL STANDARD

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Hydraulic fluid power filters — Multi-pass method for evaluating filtration performance of a filter element

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 3.

Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this International Standard may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

International Standard ISO 16889 was prepared by Technical Committee ISO/TC 131, *Fluid power systems*, Subcommittee SC 6, *Contamination control and hydraulic fluids*.

This first edition cancels and replaces ISO 4572:1981, of which it constitutes a technical revision.

Annex A forms a normative part of this International Standard. Annexes B to D are for information only.

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Introduction

In hydraulic fluid power systems, one of the functions of the hydraulic fluid is to separate and lubricate the moving parts of components. The presence of solid particulate contamination produces wear, resulting in loss of efficiency, reduced component life and subsequent unreliability.

A hydraulic filter is provided to control the number of particles circulating within the system to a level that is commensurate with the degree of sensitivity of the components to contaminant and the level of reliability required by the users.

To enable the relative performance of filters to be compared so that the most appropriate filter can be selected, test procedures should be available. The performance characteristics of a filter are a function of the element (its medium and geometry) and the housing (its general configuration and seal design).

In practice, a filter is subjected to a continuous flow of contaminant entrained in the hydraulic fluid until some specified terminal differential pressure (relief valve cracking pressure or differential pressure indicator setting) is reached.

Both the length of operating time (prior to reaching terminal pressure) and the contaminant level at any point in the system are functions of the rate of contaminant addition (ingression plus generation rates) and the performance characteristics of the filter. **TENDARD PREVIEW**

Therefore, a realistic laboratory test that establishes the relative performance of a filter should provide the test filter with a continuous supply of ingressed contaminant and allow the periodic monitoring of the filtration performance characteristics of the filter.

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The test should also provide an acceptable level of repeatability and reproducibility and a standard test contaminant [ISO medium test dust (ISO 12103-A3) in accordance with ISO 12103-1] is featured. This has been shown to have a consistent particle size distribution and is available worldwide. The filtration performance of the filter is determined by measurement of the upstream and downstream particle size distributions using automatic particle counters validated according to ISO standards.

Since it is difficult to specify, achieve and verify a cyclic flow requirement that is both realistic and consistent with the flow variations occurring in actual systems, the compromise of steady-state condition has been used for this test to enhance the repeatability and reproducibility of results.

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Hydraulic fluid power filters — Multi-pass method for evaluating filtration performance of a filter element

1 Scope

- 1.1 This International Standard specifies:
- a multi-pass filtration performance test with continuous contaminant injection for hydraulic fluid power filter elements;
- a procedure for determining the contaminant capacity, particulate removal and differential pressure characteristics;
- a test currently applicable to hydraulic fluid power filter elements that exhibit an average filtration ratio greater than or equal to 75 for particle sizes less than or equal to 25 μm(c), and a final reservoir gravimetric level of less than 200 mg/l;

NOTE The range of flows and the lower particle size limit that can be used in test facilities will be determined by validation.

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- a test using ISO medium test dust contaminant and a test fluid according to annex A.
- 1.2 This International Standard is intended to provide a test procedure that yields reproducible test data for appraising the filtration performance of a hydraulic fluid power filter element without influence of electrostatic charge.

2 Normative references

The following normative documents contain provisions which, through reference in this text, constitute provisions of this International Standard. For dated references, subsequent amendments to, or revisions of, any of these publications do not apply. However, parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent editions of the normative documents indicated below. For undated references, the latest edition of the normative document referred to applies. Members of ISO and IEC maintain registers of currently valid International Standards.

ISO 1219-1:1991, Fluid power systems and components — Graphic symbols and circuit diagrams — Part 1: Graphic symbols.

ISO 2942:1994, Hydraulic fluid power — Filter elements — Verification of fabrication integrity and determination of the first bubble point.

ISO 3722:1976, Hydraulic fluid power — Fluid sample containers — Qualifying and controlling cleaning methods.

ISO 3968:1981, Hydraulic fluid power — Filters — Evaluation of pressure drop versus flow characteristics.

ISO 4021:1992, Hydraulic fluid power — Particulate contamination analysis — Extraction of fluid samples from lines of an operating system.

ISO 4405:1991, Hydraulic fluid power — Fluid contamination — Determination of particulate contamination by the gravimetric method.

ISO 5598:1985, Fluid power systems and components — Vocabulary.

ISO 11171:1999, Hydraulic fluid power — Calibration of liquid automatic particle counters.

ISO 11943:1999, Hydraulic fluid power — On-line automatic particle-counting systems for liquids — Methods of calibration and validation.

ISO 12103–1:1997, Road vehicles — Test dust for filter evaluation — Part 1: Arizona test dust.

ASTM D 4308-95, Standard test method for electrical conductivity of liquid hydrocarbons by precision meter.

3 Terms and definitions

For the purposes of this International Standard, the terms and definitions given in ISO 5598 and the following apply.

3.1

contaminant mass injected

mass of specific particulate contaminant injected into the test circuit to obtain the terminal Δp

3.2

differential pressure

 Δp

difference between the tested component inlet and outlet pressure as measured under the specified conditions

See Figure 1.

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3.2.1

clean assembly differential pressure

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difference between the tested component inlet and outlet pressure as measured with a clean filter body containing a clean filter element 6fdb91ae75be/sist-iso-16889-2001

See Figure 1.

3.2.2

clean element differential pressure

differential pressure of the clean element calculated as the difference between the clean assembly Δp and the housing

See Figure 1.

3.2.3

final assembly differential pressure

assembly differential pressure at end of test equal to sum of housing plus terminal element differential pressures

See Figure 1.

3.2.4

housing differential pressure

differential pressure of the filter body without an element

See Figure 1.

3.2.5

terminal element differential pressure

maximum differential pressure across the filter element as designated by the manufacturer to limit useful performance

See Figure 1.

3.3

rest conductivity

electrical conductivity at the initial instant of current measurement after a d.c. voltage is impressed between electrodes

NOTE It is equal to the reciprocal of the resistance of uncharged fluid in the absence of ionic depletion or polarization.

3.4

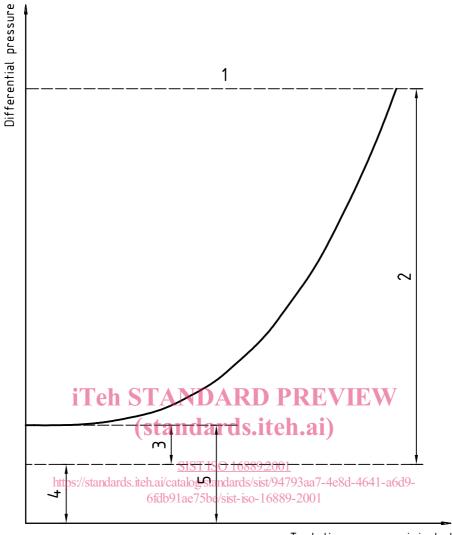
retained capacity

mass of specific particulate contaminant effectively retained by the filter element when terminal element Δp is reached

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Test time or mass injected

Key

- 1 Final assembly (end of test) differential pressure
- 2 Terminal element differential pressure
- 3 Clean element differential pressure
- 4 Housing differential pressure
- 5 Clean assembly differential pressure

Figure 1 — Differential pressure conventions for multi-pass test

4 Symbols

4.1 Graphic symbols

Graphic symbols used are in accordance with ISO 1219-1.

4.2 Quantity symbols

Reference	Symbol	Units	Description or explanation
4.2.1	$\overline{A}_{\mathbf{u},x}$	part/ml	Overall average upstream count > size x
4.2.2	$\overline{A}_{d,x}$	part/ml	Overall average downstream count > size x
4.2.3 ^a	$eta_{x(c)}$	None	Filtration ratio at particle size <i>x</i> (ISO 11171 calibration)
4.2.4	$\beta_{x,t}$	None	Filtration ratio at particle size x and time interval t
4.2.5 ^a	$\overline{eta}_{x(c)}$	None	Average filtration ratio at particle size <i>x</i> (ISO 11171 calibration)
4.2.6	C_{R}	g	Retained capacity
4.2.7	G_{b}	mg/l	Average base upstream gravimetric level
4.2.8	$G_{b}{}'$	mg/l	Desired base upstream gravimetric level
4.2.9	G_{i}	mg/l	Average injection gravimetric level
4.2.10	G_{i}'	mg/l	Desired injection gravimetric level
4.2.11	G ₈₀	mg/l	Test reservoir gravimetric level at 80 % assembly Δp
4.2.12	М	g	Mass of contaminant needed for injection
4.2.13	M_{e}	g	Estimated filter element capacity (mass injected)
4.2.14	M_{I}	g	Contaminant mass injected
4.2.15	M_p	g	Contaminant mass injected at element differential pressure Δp
4.2.16	n	none	Number of counts in specific time period
4.2.17	$N_{u,x,i}$	part/ml	Number of upstream particles > size x at count i
4.2.18	$N_{d,x,i}$	part/ml	Number of downstream particles > size x at count i
4.2.19	$\overline{\overline{N}}_{u,x,t}$	part/ml (Stan	Average upstream count > size x at time interval t
4.2.20	$\overline{\overline{N}}_{d,x,t}$	part/ml	Average downstream count $>$ size x at time interval t
4.2.21	<i>p</i>	Pa, kPa or bar S	Pressure 889:2001
4.2.22	Δp	Pa, kPa or bar	Differential pressure (2) (2) (2) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4
4.2.23	q	I/min	Test flow rate
4.2.24	q_d	I/min	Discarded downstream sample flow rate
4.2.25	q_{i}	l/min	Average injection flow rate
4.2.26	${q_{i}}'$	I/min	Desired injection flow rate
4.2.27	$q_{\sf u}$	I/min	Discarded upstream sample flow rate
4.2.28	t	min	Test time
4.2.29	t'	min	Predicted test time
4.2.30	t_{f}	min	Final test time
4.2.31	t_p	min	Test time at element differential pressure Δp
4.2.32	V_{if}	I	Final measured injection system volume
4.2.33	V_{ii}	1	Initial measured injection system volume
4.2.34	V_{min}	1	Minimum required operating injection system volume
4.2.35	V_{tf}	I	Final measured filter test system volume
4.2.36	$V_{\sf v}$	1	Minimum validated injection system volume

^a The subscript (c) signifies that the filtration ratio, $\beta_{x(c)}$, and the average filtration ratio, $\overline{\beta}_{x(c)}$, are based on this standard test method (ISO 16889) using particle counters calibrated in accordance with ISO 11171.

5 General procedure

- **5.1** Set up and maintain apparatus in accordance with clause 6 and clause 7.
- **5.2** Validate equipment in accordance with clause 8.
- **5.3** Run all tests in accordance with clauses 9, 10 and 11.
- **5.4** Analyse test data in accordance with clause 12.
- **5.5** Present data from clauses 10, 11 and 12 in accordance with clause 13.

6 Test equipment

- 6.1 Suitable timer.
- **6.2** Automatic particle counter(s), calibrated in accordance with ISO 11171.
- **6.3 ISO medium test dust (ISO 12103-A3),** in accordance with ISO 12103-1, dried at 110 °C to 150 °C for not less than 1 h for quantities less than 200 g and for use in the test system, mix in the test fluid, mechanically agitate, then disperse ultrasonically with a power density of 3 000 W/m² to 10 000 W/m².

NOTE This dust is commercially available. For availability of ISO 12103-A3 test dust, contact the ISO secretariat service or national members of ISO.

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- **6.4 Online counting system**, and **dilution system** if necessary, that has been validated in accordance with ISO 11943.
- **6.5** Sample bottles containing less than 20 particles per milliture of bottle volume greater than 6 μm(c), as qualified in accordance with ISO 3722 to collect samples for gravimetric analyses. 41-a6d9-6fdb9 (ac 75be/sist-iso-16889-200)
- **6.6** Petroleum base test fluid in accordance with annex A.
- NOTE 1 The use of this carefully controlled hydraulic fluid assures greater reproducibility of results and is based upon current practices, other accepted filter standards and its world-wide availability.
- NOTE 2 If an anti-static agent is added to this test fluid it may affect the test results.
- **6.7** Filter performance test circuit comprised of a "filter test system" and a "contaminant injection system".
- **6.7.1** Filter test system consisting of:
- a) a reservoir, pump, fluid conditioning apparatus and instrumentation that are capable of accommodating the range of flows, pressures and volumes required by the procedure and is capable of meeting the validation requirements of clause 8;
- b) a clean-up filter capable of providing an initial system contamination level as specified in Table 2:
- c) a configuration that is relatively insensitive to the intended operative contaminant level;
- d) a configuration that will not alter the test contaminant distribution over the anticipated test duration;
- e) pressure taps in accordance with ISO 3968;
- f) fluid sampling sections upstream and downstream of the test filter in accordance with ISO 4021.

NOTE For typical configurations that have proved to be satisfactory refer to annex B.

6.7.2 Contaminant injection system consisting of:

- a) a reservoir, pump, fluid conditioning apparatus and instrumentation that are capable of accommodating the range of flows, pressures and volumes required by the procedure and is capable of meeting the validation requirements of clause 8;
- b) a configuration that is relatively insensitive to the intended operative contaminant level;
- c) a configuration that will not alter the test contaminant distribution over the anticipated test duration;
- d) a fluid sampling section in accordance with ISO 4021.
- NOTE For typical configurations that have proven to be satisfactory, refer to annex B.
- **6.8 Membranes and associated laboratory equipment** suitable for conducting the gravimetric method in accordance with ISO 4405.

7 Accuracy of measurements and test conditions

- 7.1 Utilize and maintain instrument accuracy and test conditions within the limits given in Table 1.
- **7.2** Maintain specific test parameters within the limits given in Table 2 depending on the test condition being conducted.

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Table 1 — Instrument accuracy and test condition variation

Test parameter	SIST ISO 16889:20	Instrument accuracy (±) 01 of reading	Allowed test condition variation (±)
Conductivity https://standards.iteh.a	i/catalog/standards/sist/9 ilb91ae75bS/sst-iso-168	4793aa7-4e8d-4641-ad 89-2001 10 %	5d9-
Differential pressure	PA, kPa or bar	5 %	_
Base upstream gravimetric	mg/l	_	10 %
Flow:			
Injection flow	ml/min	2 %	5 %
Test flow	l/min	2 %	5 %
APC sensor flow	l/min	1,5 %	3 % ^a
Kinematic viscosity ^b	mm²/s	2 %	1 mm ² /s
Mass	g	0,1 mg	_
Temperature	°C	1 °C	2 °C °
Time	S	1 s	_
Volume:			
Injection system	I	2 %	
Filter test system	I	2 %	5 %

a Sensor flow variation to be included in the overall 10 % allowed between sensors.

b $1 \text{ mm}^2/\text{s} = 1 \text{ cSt (centistoke)}.$

Or as required to guarantee the viscosity tolerance.